



확장칼만필터링 항해 데이터를 활용한 선박에 작용하는 유체력 추정용 물리기반 신경추정기(PINE)

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A Physics-Informed Neural Estimator (PINE) for Ship Hydrodynamic Forces using EKF-processed Voyage Data

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Accurate estimation of hydrodynamic forces is essential for ship motion modeling and performance monitoring, but these forces cannot be directly measured during voyages. The Extended Kalman Filter (EKF) can estimate them from ship state data, but its accuracy is limited by linearization errors and noise-tuning sensitivity. This paper presents PINE, a Physics-Informed Neural Estimator combining EKF and a Physics-Informed Neural Network (PINN), in which voyage-derived ship states are transformed to the body-fixed frame and fed into both models. The EKF generates pseudo-labels used as supervised targets in the PINN data loss, while a physics loss enforces consistency with the equations of motion. Two configurations are compared: PINE(L_p), using only the physics loss, and PINE(L_p+L_d), the proposed framework, using the full combined loss. PINE is first validated on simulation data with ground-truth forces, trained on the 10° -10° zigzag dataset and tested on the 20° -20° zigzag dataset. PINE(L_p+L_d) achieves higher R^2 and lower Normalized Root Mean Square Error (NRMSE) than EKF and PINE(L_p). Applied to real voyage data without ground truth, PINE(L_p+L_d) confirms practical applicability, offering a physically consistent method deployable for real-time onboard force estimation without retraining.

Keywords : Hydrodynamic force estimation, Physics-Informed Neural Network (PINN), Extended Kalman Filter (EKF), Voyage data

1. Introduction

Hydrodynamic forces acting on a ship, including surge force, sway force, and yaw moment, govern ship motion such as maneuvering, course-keeping, and dynamic stability. Accurate knowledge of these forces is essential for ship performance monitoring, fuel optimization, and autonomous navigation (Fossen, 2011). Traditionally, these forces are obtained from captive model tests in a towing tank or Computational Fluid Dynamics simulations (Nguyen et al., 2022; Park et al., 2020;

Choi et al., 2022; Mai et al., 2022), but scale effects introduce uncertainties in full-scale predictions (Terziev et al., 2022). This has motivated researchers to estimate hydrodynamic forces directly from full-scale sea trial data (You, 2019; Park and Lee, 2020; Jeon et al., 2021), leading to methods such as the Estimation-Before-Modeling (EBM) approach (Yoon and Rhee, 2003), which uses the Extended Kalman Filter (EKF) combined with the Modified Bryson-Frazier (MBF) smoother. The MBF smoother refines the EKF forward estimates by performing a backward pass over the entire dataset, improving estimation

accuracy. However, this requires the full dataset to be available in advance, making it a batch processing method that cannot operate in real time. Furthermore, the MBF smoother depends entirely on the EKF forward pass and inherits its linearization errors. These limitations restrict the applicability of the MBF approach for onboard deployment.

In parallel, recent data-driven approaches, including deep learning models using Automatic Identification System data (Li et al., 2023; Zhang et al., 2023) and Physics-Informed Neural Networks (PINNs) (Raissi et al., 2019), have shown promising results in ship motion modeling. PINNs in particular embed physical laws into the training process and have been applied to USV dynamics (Xu et al., 2022) and autonomous ship digital twins (Xia et al., 2024). However, PINN training without a supervisory signal is unreliable, and EKF accuracy is limited by linearization errors and noise covariance tuning. These two approaches have not been combined to estimate hydrodynamic forces directly from voyage data without dedicated maneuvers or ground-truth force measurements.

This paper proposes PINE, a Physics-Informed Neural Estimator that combines EKF and PINN to address this gap. The EKF is used to generate pseudo-labels as supervised training targets in the data loss term, while the MBF smoother is replaced by a PINN that enforces consistency with the ship equations of motion through a physics loss based on finite difference derivatives of the measured ship states. The main contributions are: (1) a framework combining EKF pseudo-label generation with PINN training for hydrodynamic force estimation from voyage data; (2) a combined loss function integrating EKF pseudo-labels as data supervision and ship equations of motion as physics constraints; and (3) validation on simulation data using R^2 and NRMSE, followed by application to real voyage data.

2. Methodology

2.1 Ship dynamic model

Two coordinate frames are used in this study, as shown in Fig. 1. The Earth-fixed coordinate system ($O-xy$) has its origin fixed on the Earth's surface, with the x -axis pointing toward North and the y -axis pointing toward East. The body-fixed coordinate system ($o-x_b y_b$) has its origin located at the ship's center of gravity, with the x_b -axis pointing toward the bow and the y_b -axis pointing toward the starboard side. The heading angle ψ is defined as the angle from the x -axis to the x_b -axis, measured clockwise.

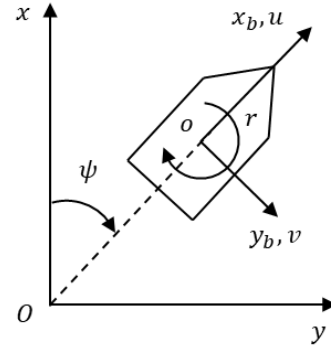


Fig. 1 Earth-fixed and body-fixed coordinate systems

The ship maneuvering motion is described using a 3-DOF model in the horizontal plane, considering surge, sway, and yaw motions. Following the MMG standard method (Yasukawa and Yoshimura, 2015), the equations of motion in the body-fixed coordinate system are expressed as:

$$m(\dot{u} - vr - x_G r^2) = X \quad (1)$$

$$m(\dot{v} + ur + x_G \dot{r}) = Y \quad (2)$$

$$I_{zz} \dot{r} + m x_G (\dot{v} + ur) = N \quad (3)$$

where m is the ship mass, I_{zz} is the moment of inertia about the vertical axis, and x_G is the longitudinal position of the center of gravity. u and v denote the surge and sway velocities in the body-fixed frame, and r is the yaw rate. The term $\dot{u}$, $\dot{v}$, and $\dot{r}$ represent their time derivatives, respectively, while X , Y , N are the total hydrodynamic forces and moment acting on the ship.

2.2 Coordinate transformation

Voyage data recorded by the onboard measurement system contains: Latitude, Longitude, Speed Over Ground (SOG), Course Over Ground (COG), Heading (HDG), and Rate Of Turn (ROT). Latitude and Longitude are converted to Cartesian coordinates x and y in the Earth-fixed frame using the Universal Transverse Mercator (UTM) projection, providing position coordinates in meters. SOG and COG describe the magnitude and direction of the ship's velocity vector over ground, while HDG represents the direction the bow is pointing. The difference between COG and HDG arises from the effects of wind, waves, and ocean currents. The yaw rate r and heading angle ψ are directly obtained

from ROT and HDG, respectively. The surge velocity u and sway velocity v are obtained by projecting the SOG vector onto the body-fixed axes as follows (Inazu et al., 2020):

$$u = SOG \times \cos(COG - HDG) \quad (4)$$

$$v = SOG \times \sin(COG - HDG) \quad (5)$$

2.3 EKF-based force estimation

The EKF is widely used to estimate state variables of nonlinear state-space models (Hoff, 1995). Since the algorithm is well established, only the final forms are presented here. The state vector is defined as:

$$\underline{x} = [u \ v \ r \ x \ y \ \psi \ X \ Y \ N \ \dot{X} \ \dot{Y} \ \dot{N} \ \ddot{X} \ \ddot{Y} \ \ddot{N}]^T \quad (6)$$

The hydrodynamic forces X , Y , and N are modeled as third-order Gauss-Markov model. The third-order Gauss-Markov model is adopted following Yoon and Rhee (2003), where this formulation was shown to provide sufficient flexibility to represent the time-varying behavior of hydrodynamic forces.

$$\ddot{X} = w_X, \quad \ddot{Y} = w_Y, \quad \ddot{N} = w_N \quad (7)$$

where w_X , w_Y , and w_N are independent zero-mean Gaussian white noise processes.

The measurement vector consists of quantities derived from voyage data:

$$\underline{z} = [u \ v \ r \ x \ y \ \psi]^T \quad (8)$$

The predicted covariance, Kalman gain, filtered state vector, and error covariance matrix are given by:

$$P_{k|k-1} = F_k P_{k-1|k-1} F_k^T + Q \quad (9)$$

$$K_k = P_{k|k-1} H^T (H P_{k|k-1} H^T + R)^{-1} \quad (10)$$

$$\hat{\underline{x}}_{k|k} = \hat{\underline{x}}_{k|k-1} + K_k \Delta \underline{z}_{k|k-1} \quad (11)$$

$$P_{k|k} = (I - K_k H) P_{k|k-1} \quad (12)$$

where $F_k = \partial f / \partial \underline{x} |_{\hat{\underline{x}}_{k-1|k-1}}$ is the Jacobian of the nonlinear state transition function f . H is the Jacobian matrix of $\underline{z}$, I

is the identity matrix, Q is the process noise covariance matrix, and R is the measurement noise covariance matrix. Both Q and R are assumed to be diagonal. The elements of R can be estimated from the variance of the measured data, while the elements of Q are more difficult to determine and are obtained by iterative tuning until satisfactory filter performance is achieved (Hoff, 1995).

2.4 PINN-based force estimation

PINNs incorporate physical constraints into the neural network training process through a physics-based loss function, allowing the model to learn from data while remaining consistent with the governing equations (Raissi et al., 2019). In this study, the PINN is implemented as a fully connected feedforward neural network following the formulation of Xu et al. (2022). While the EKF requires manual tuning of the noise covariance matrices Q and R , the PINN architecture is systematically determined through grid search hyperparameter optimization (Jaber et al., 2025). The search covers the number of hidden layers, neurons per layer, and activation function.

In this study, the network takes six ship state variables $[u, v, r, x, y, \psi]$ as input and produces the three estimated hydrodynamic forces $[\hat{X}, \hat{Y}, \hat{N}]$ as output. The network is trained by minimizing a total loss function, which includes:

$$L = \lambda_d L_d + \lambda_p L_p \quad (13)$$

where λ_d and λ_p are the weights that balance the contribution of the data loss and physics loss, respectively. In this study, both weights are set to 1.0, consistent with the original PINN formulation of Raissi et al. (2019). This choice is justified by the fact that both loss terms are computed as MSE over the same dataset and share the same physical units, making their magnitudes naturally comparable (Rohrhofer et al., 2023). The total loss is minimized using the Adam optimizer. The data loss measures the difference between the PINN output and the EKF pseudo-labels:

$$L_d = \frac{1}{N} \sum_{k=1}^N [(\hat{X}_k - \tilde{X}_k)^2 + (\hat{Y}_k - \tilde{Y}_k)^2 + (\hat{N}_k - \tilde{N}_k)^2] \quad (14)$$

where $\tilde{X}_k$, $\tilde{Y}_k$, $\tilde{N}_k$ are the EKF pseudo-labels at time step k . The physics loss enforces consistency with Eqs. (1)–(3):

$$L_p = \frac{1}{N} \sum_{k=1}^N [(\hat{X}_k - X_k)^2 + (\hat{Y}_k - Y_k)^2 + (\hat{N}_k - N_k)^2] \quad (15)$$

where X_k , Y_k , N_k are the forces and moment computed from Eqs. (1)–(3) using the measured states. The time derivatives $\dot{u}$, $\dot{v}$, and $\dot{r}$ are computed numerically using finite differences with a fixed time step of 0.1 s for simulation data and 1 s for voyage data.

2.5 PINE framework

The overall PINE framework is shown in Fig. 2. The framework consists of two stages: training and testing. In the training stage, ship state variables are fed into the EKF to generate pseudo-labels $\tilde{X}$, $\tilde{Y}$, and $\tilde{N}$. These pseudo-labels, together with the ship states, are used to train the PINN by minimizing the total loss L defined in Eq. (13). The trained model is saved for use in the testing stage. In the testing stage, the trained PINN takes unseen ship state variables as input and produces the estimated hydrodynamic forces $\hat{X}$, $\hat{Y}$, and $\hat{N}$ as output.

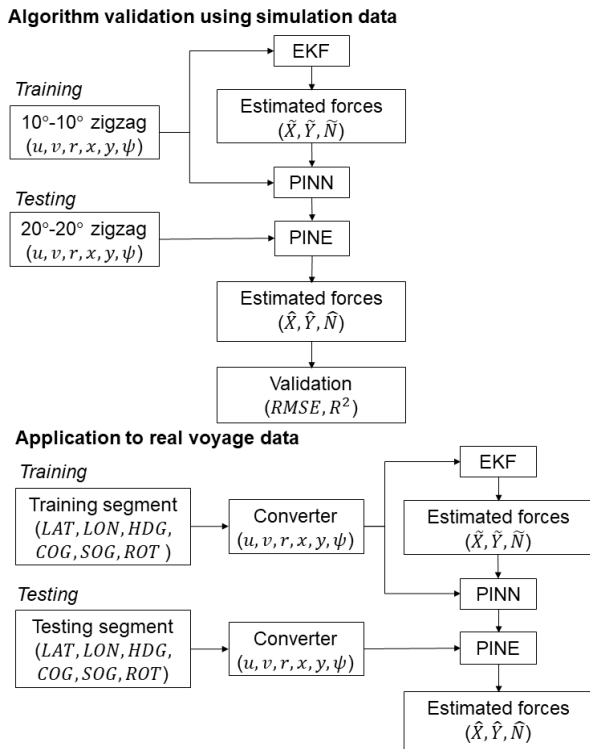


Fig. 2 Overall framework of the proposed PINE method

The framework is applied in two scenarios. In the first scenario, PINE is trained on simulation data from a 10°–10° zigzag test and tested on a 20°–20° zigzag test, where ground-truth forces are available for validation using R² and NRMSE. Both PINE(L_p) and PINE($L_p + L_d$) are evaluated to

quantify the contribution of EKF pseudo-labels to training performance. Note that the EKF pseudo-labels inherently contain estimation errors due to linearization and correction of the noise covariance matrix, which are directly propagated into the training process through the data loss term L_d . While these errors may affect the training process, the physics loss term L_p simultaneously enforces consistency with the ship equations of motion, preventing the estimator from overfitting to inaccurate pseudo-labels. The 10°–10° zigzag test is selected for training because it provides sufficient excitation of the ship dynamics, while the 20°–20° zigzag test is used for testing to evaluate the generalization ability of the trained model. In the second scenario, PINE($L_p + L_d$) is trained on a segment of real voyage data and tested on another segment, where no ground-truth forces are available. For real voyage data, the coordinate transformation described in Section 2.2 is applied to convert the measured quantities LAT, LON, HDG, COG, SOG, and ROT into the body-fixed state variables (u, v, r, x, y, ψ) before being fed into the EKF and PINN.

A key advantage of PINE is that the EKF provides a physically informed supervisory signal when no ground-truth force measurements are available, while the PINN produces improved estimates beyond the limitations of the EKF alone. Once trained, the model can be deployed directly on a ship's onboard system for real-time estimation without retraining, and can be fine-tuned for other ships using transfer learning (Pan and Yang, 2010).

3. Simulation validation

The simulation dataset is generated by numerically solving the MMG standard equations of motion (Yasukawa and Yoshimura, 2015) in three degrees of freedom, with hydrodynamic forces decomposed into hull, propeller, and rudder contributions. The hydrodynamic coefficients are taken from Nguyen et al. (2022), estimated through captive model tests in a towing tank. All simulations are performed at full scale for the Korea Autonomous Surface Ship (KASS) at its design speed of 15.5 kn. The principal particulars of KASS are listed in Table 1.

Two maneuvering scenarios are considered: the 10°–10° and 20°–20° zigzag tests, and the corresponding simulated ship states are shown in Fig. 3. The 10°–10° zigzag dataset is used for EKF-based force estimation, hyperparameter optimization, and PINN training because it best represents the typical dynamic range of a large ship during voyage. This

Table 1 Principal particulars of KASS

Item	Unit	Full scale	Model scale
Scale ratio	–	1	81.78
Length, L	m	163.55	2.00
Breadth, B	m	44.60	0.55
Draft, T	m	9.32	0.11
Ship mass, m	kg	3.65×10^7	66.77
Center of gravity, x_G	m	0.00	0.00
Radius of gyration, k_{zz}	m	53.97	0.66

dataset is divided into a training set (75%) and a validation set (25%) in chronological order to preserve the temporal structure of the data and avoid data leakage. The 20°–20° zigzag dataset is used to assess the generalizability of the trained model because it involves larger rudder angles that were not encountered during training.

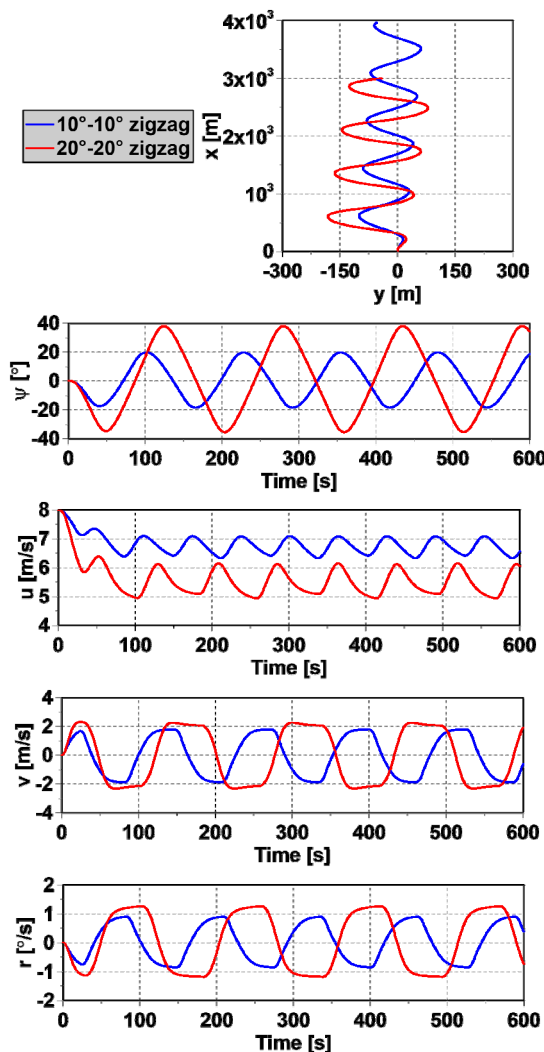


Fig. 3 Simulated ship states for 10°–10° and 20°–20° zigzag tests

The EKF is applied to the 10°–10° zigzag data to generate pseudo-labels. Fig. 4 shows the estimated hydrodynamic forces $\tilde{X}$, $\tilde{Y}$, and $\tilde{N}$ from the EKF compared against the simulation ground truth for the 10°–10° zigzag test. The EKF achieves reasonable accuracy for $\tilde{Y}$ and $\tilde{N}$, with R^2 of 0.976 and 0.948 and NRMSE of 0.156 and 0.227, respectively. However, the estimation of $\tilde{X}$ remains limited, with R^2 of 0.572 and NRMSE of 0.652. Despite this limitation, the EKF estimates are used as pseudo-labels for PINE($L_p + L_d$) training, where the combined loss helps reduce the effect of linearization errors through physics-constrained learning. In addition, since the PINN takes the directly measured ship states (u , v , r , x , y , ψ) as input, the coupling between force components through the drift angle is correctly preserved regardless of EKF estimation accuracy.

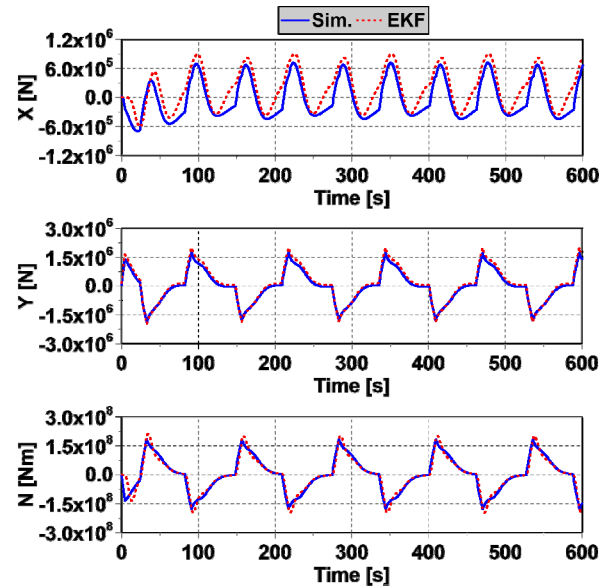


Fig. 4 Hydrodynamic force estimation for 10°–10° zigzag

A grid search is performed to identify the optimal PINN architecture (Jaber et al., 2025). The search covers the number of epochs {500, 1000, 1500, 2000, 2500, 3000}, hidden layers {1, 2, 3, 4, 5}, neurons per layer {3, 6, 9, 12, 15}, and activation functions {linear, tanh, ReLU, sigmoid}. For each configuration, the average NRMSE across the three force components $\hat{X}$, $\hat{Y}$, and $\hat{N}$ is computed on the validation set as the selection criterion. Table 2 summarizes selected representative results, chosen to illustrate the individual effect of each hyperparameter while holding the others fixed. The optimal architecture consists of 5 hidden layers, 15 neurons per layer, tanh activation, and 3000 epochs, yielding the lowest average NRMSE and is therefore adopted for all subsequent training.

Table 2 PINE architecture optimization for simulation data

Hidden layer	Neuron	Activation	Epoch	Val. loss
1	15	tanh	3000	0.737
3	15	tanh	3000	0.754
5	15	tanh	3000	0.070
5	15	ReLU	3000	0.088
5	15	sigmoid	3000	0.420
5	15	tanh	1000	0.105
5	15	tanh	2000	0.103

Using the optimal configuration, two training configurations are compared as an ablation study: PINE(L_p), which minimizes only the physics loss, and PINE(L_p+L_d), which minimizes the combined loss as defined in Eq. (13). In both configurations, the EKF is applied to generate pseudo-labels, the distinction lies solely in whether these pseudo-labels are incorporated as supervised training targets in the loss function. The training loss for each configuration is computed as the RMSE between the predicted and ground-truth hydrodynamic forces on the validation set. Fig. 5 shows the training loss convergence for both configurations. At epoch 3000, PINE(L_p) achieves a final loss of 1.112×10^{-2} while PINE(L_p+L_d) reaches 2.063×10^{-3} . The latter converges faster and to a lower final value, indicating that directly incorporating EKF pseudo-labels into the loss function effectively accelerates and stabilizes training.

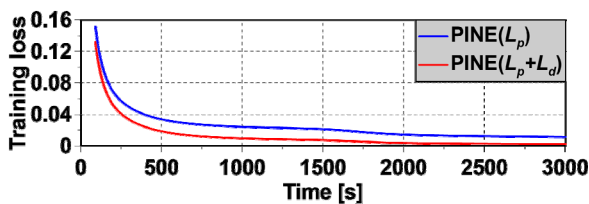


Fig. 5 Training loss for simulation data

The trained models are then applied directly to the 20°–20° zigzag ship states without retraining. Fig. 6 shows the estimated hydrodynamic forces from EKF, PINE(L_p), and PINE(L_p+L_d) compared to the simulation ground truth. The EKF produces good estimates for $\tilde{Y}$ and $\tilde{N}$, but shows larger errors for $\tilde{X}$. PINE(L_p) produces accurate estimates for all three force components. PINE(L_p+L_d) further improves upon both methods and produces the closest agreement with the ground truth across all force components. Table 3 provides a quantitative comparison. PINE(L_p+L_d) achieves the highest R^2 and the lowest NRMSE for all force

components. The most notable improvement is observed for $\hat{X}$, where R^2 increases from 0.820 for EKF and 0.951 for PINE(L_p) to 0.997, while NRMSE reduces from 0.423 and 0.220 to 0.053. For $\hat{Y}$ and $\hat{N}$, all three methods perform well, but PINE(L_p+L_d) still achieves further improvement.

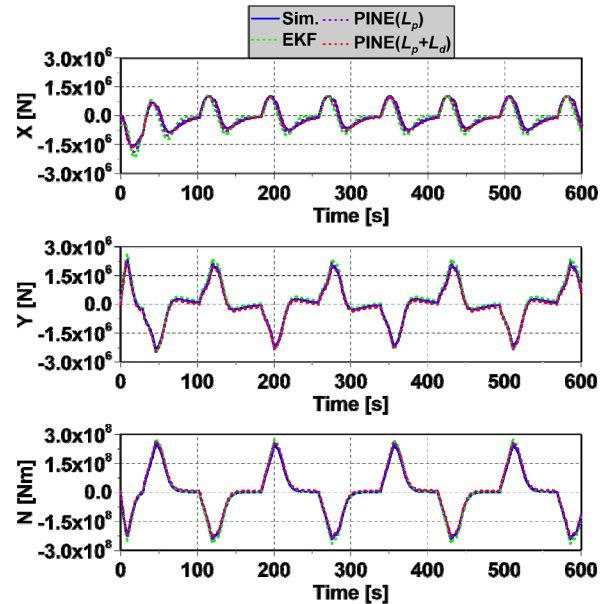


Fig. 6 Hydrodynamic force estimation for 20°–20° zigzag

Table 3 Hydrodynamic force estimation performance for 20°–20° zigzag

Force	EKF		PINE(L_p)		PINE(L_p+L_d)	
	R^2	NRMSE	R^2	NRMSE	R^2	NRMSE
X	0.820	0.423	0.951	0.220	0.997	0.053
Y	0.978	0.147	0.991	0.095	0.997	0.050
N	0.990	0.100	0.994	0.074	0.996	0.062

The advantage of PINE(L_p+L_d) becomes more important when applied to real voyage data, where no ground-truth force measurements are available. In this case, PINE(L_p) relies solely on the physics loss and receives no data-driven supervision, which limits its reliability. By contrast, PINE(L_p+L_d) leverages EKF pseudo-labels as a supervisory signal, enabling stable and accurate training even without ground-truth measurements. For this reason, only PINE(L_p+L_d) is applied in the real voyage data application.

4. Application to Voyage data

The voyage data used in this study were recorded by the onboard measurement system of KASS during a voyage from

the Incheon area to the Busan area along the western and southern coast of Korea. The data spans from 2025-05-17 to 2025-05-20, with a total duration of approximately 66 hours and a sampling interval of 1 second. The training and testing segments are selected based on data quality and continuity, prioritizing periods with stable sensor recordings and sufficient maneuver variation. The training segment spans 2025-05-17 22:30 to 2025-05-18 10:50 (approximately 12.3 hours), and the testing segment spans 2025-05-18 13:23 to 2025-05-19 04:10 (approximately 14.8 hours). A gap of approximately 2.5 hours between the two segments, during which the data logging system was temporarily interrupted, was excluded from the analysis. The coordinate transformation described in Section 2.2 is applied to convert the measured quantities LAT, LON, HDG, COG, SOG, and ROT into the body-fixed state variables (u, v, r, x, y, ψ) . The transformed state variables for both the training and testing segments are shown in Fig. 7.

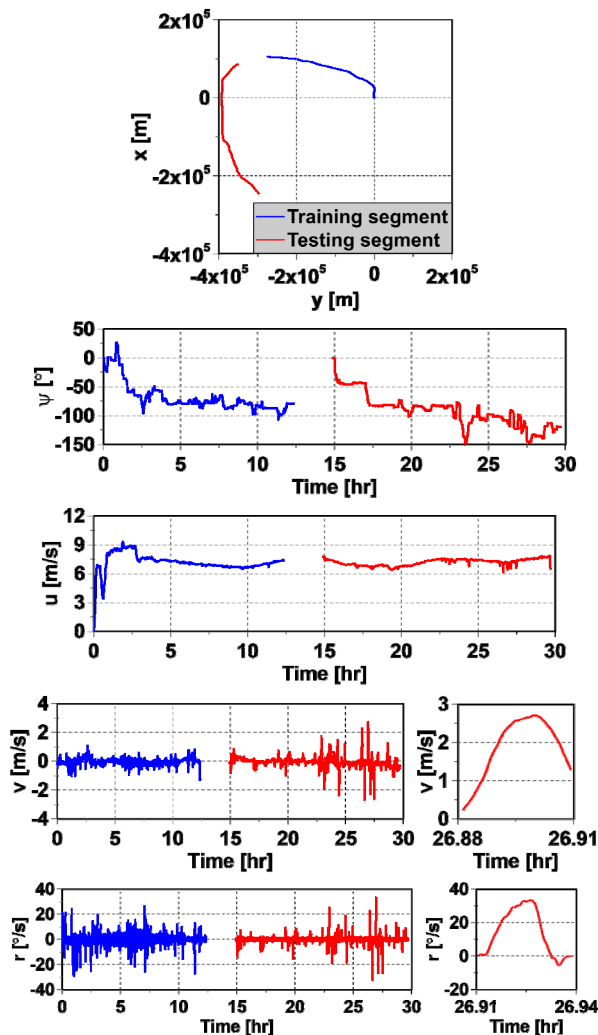


Fig. 7 Transformed ship states for voyage data

Although v and r in Fig. 7 appear noisy due to the compression of approximately 30 hours of data into a single figure, the fluctuations reflect real physical variations caused by continuous rudder adjustments rather than measurement noise. As shown in the insets, both data vary smoothly at the sampling time of 1 second. Therefore, the finite difference approximations of $\dot{u}$, $\dot{v}$, and $\dot{r}$ represent actual ship accelerations, and the resulting forces X_k , Y_k , and N_k computed from Eqs. (1)–(3) provide physically meaningful constraints for the physics loss term L_p in Eq. (15).

The EKF is applied to the training segment to generate pseudo-labels $\tilde{X}$, $\tilde{Y}$, and $\tilde{N}$. Since no ground-truth force measurements are available for real voyage data, the quality of the EKF estimates cannot be directly evaluated. However, as demonstrated in the simulation validation in Section 3, the EKF provides reasonable force estimates that serve as an effective supervisory signal for $\text{PINE}(L_p+L_d)$ training, with the physics loss independently compensating for linearization errors.

A grid search is performed to identify the optimal PINN architecture for the voyage data, following the same procedure as in Section 3, with neurons per layer extended to $\{16, 32, 64, 128, 256\}$ to account for the increased complexity of real voyage data. Since no ground-truth forces are available, the validation loss is computed as the sum of the data loss and physics loss on a validation data (25%) of the training segment. Table 4 presents selected representative results. The optimal architecture consists of 3 hidden layers, 32 neurons per layer, tanh activation, and 3000 epochs, yielding the lowest validation loss.

Table 4 PINE architecture optimization for voyage data

Hidden layers	Neurons	Activation	Epochs	Val. loss
1	32	tanh	3000	8.834
3	32	tanh	3000	0.471
5	32	tanh	3000	0.561
3	64	tanh	3000	1.298
3	32	ReLU	3000	2.024
3	32	tanh	1000	1.348

Using the optimal configuration, the training loss convergence of $\text{PINE}(L_p+L_d)$ is shown in Fig. 8. The model converges steadily and reaches a low final validation loss at epoch 3000, consistent with the simulation results in Section 3. This confirms that EKF pseudo-labels provide an effective supervisory signal for PINN training even when no ground-truth force measurements are available.

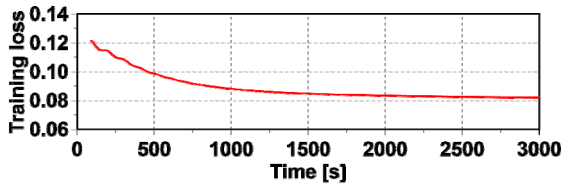


Fig. 8 Training loss for voyage data

The trained $\text{PINE}(L_p+L_d)$ model is applied to the testing segment to estimate the hydrodynamic forces. The results are shown in Fig. 9, alongside the EKF estimates for comparison. Although ground-truth force measurements are unavailable for direct validation, several observations can be made. For $\hat{X}$, both methods produce positive estimates consistent with the resistive nature of surge force during forward motion. After hour 8 of the testing segment (corresponding to hour 23 of the full voyage record in Fig. 7), ψ changes from -90° to -150° (counterclockwise), inducing a negative yaw rate r of approximately $-10^\circ/\text{s}$ and larger oscillations in v of approximately 2 m/s while u remains stable at approximately 7 m/s. Since $\dot{u}$ is approximately zero, Eq. (1) gives $X \approx m(-vr - x_G r^2)$, where the term $-vr$ becomes positive with $r < 0$, explaining the upward drift in $\hat{X}$ estimated by $\text{PINE}(L_p+L_d)$. For $\hat{Y}$, the dominant term ur in Eq. (2) becomes negative with $u > 0$ and $r < 0$, explaining the opposing downward drift observed in both $\text{PINE}(L_p+L_d)$ and EKF estimates. For $\hat{N}$, both methods produce estimates that oscillate around zero throughout the testing segment, consistent with the periodic nature of yaw motion during a

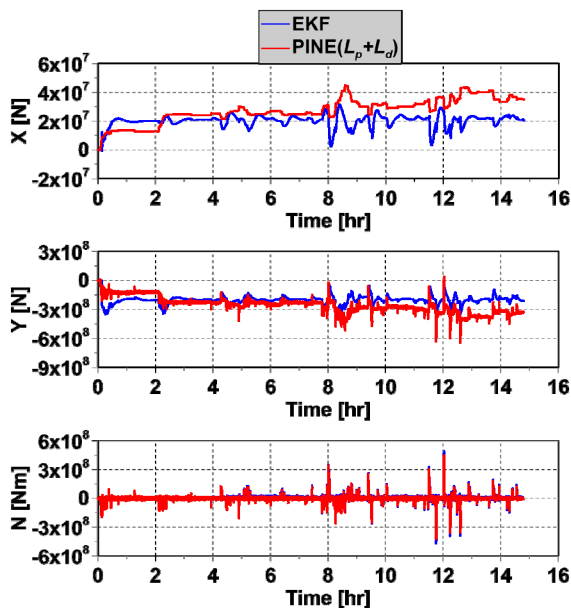


Fig. 9 Hydrodynamic force estimation for testing segment

long-distance voyage. Overall, $\text{PINE}(L_p+L_d)$ captures the general trends of all three force components, demonstrating its practical applicability for hydrodynamic force estimation from real voyage data.

5. Conclusion

This paper proposed PINE, a Physics-Informed Neural Estimator that integrates the EKF and PINN for hydrodynamic force estimation from voyage data. The EKF generates pseudo-labels as supervised training targets, while the physics loss independently enforces consistency with the ship equations of motion through automatic differentiation.

Validation on simulation data demonstrated that $\text{PINE}(L_p+L_d)$ consistently outperforms both the standalone EKF and $\text{PINE}(L_p)$ across all three force components. For the 20° - 20° zigzag generalization test, $\text{PINE}(L_p+L_d)$ achieved R^2 of 0.997, 0.997, and 0.996 with NRMSE of 0.053, 0.050, and 0.062 for surge force, sway force, and yaw moment, respectively. The framework was further applied to real voyage data from KASS, where the estimated forces capture the general trends of all three force components, confirming its practical applicability without requiring dedicated sea trial maneuvers or ground-truth force measurements.

The current study has several limitations. First, the framework is validated on a single ship type (KASS) and a limited set of maneuvers. Second, the EKF requires manual tuning of Q and R , which may affect pseudo-label quality. Third, environmental disturbances such as wind, waves, and ocean currents are not accounted for, which may introduce bias in the velocity estimates from COG and SOG data. Fourth, periodic model updating may be necessary for long-duration deployments. Future work will address these limitations by extending the framework to additional ship types, incorporating automatic noise tuning, integrating environmental disturbance models, performing indirect validation of the estimated forces through hydrodynamic coefficient identification, and conducting a quantitative comparison with the MBF smoother to characterize the trade-off between real-time capability and batch estimation accuracy. In addition, more efficient hyperparameter tuning approaches beyond grid search will be investigated.

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Authorship Contribution Statement

Hoang Thien Vu: Conceptualization, Formal analysis, Funding acquisition, Investigation, Methodology, Writing – original draft; **Jeonghong Park:** Data curation, Project administration, Supervision; **Hyeon Kyu Yoon:** Conceptualization, Project administration, Supervision, Validation, Writing – review & editing.



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